

# From micro to macro: material degradation modeling and failure prediction using microstructure images

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# Outline

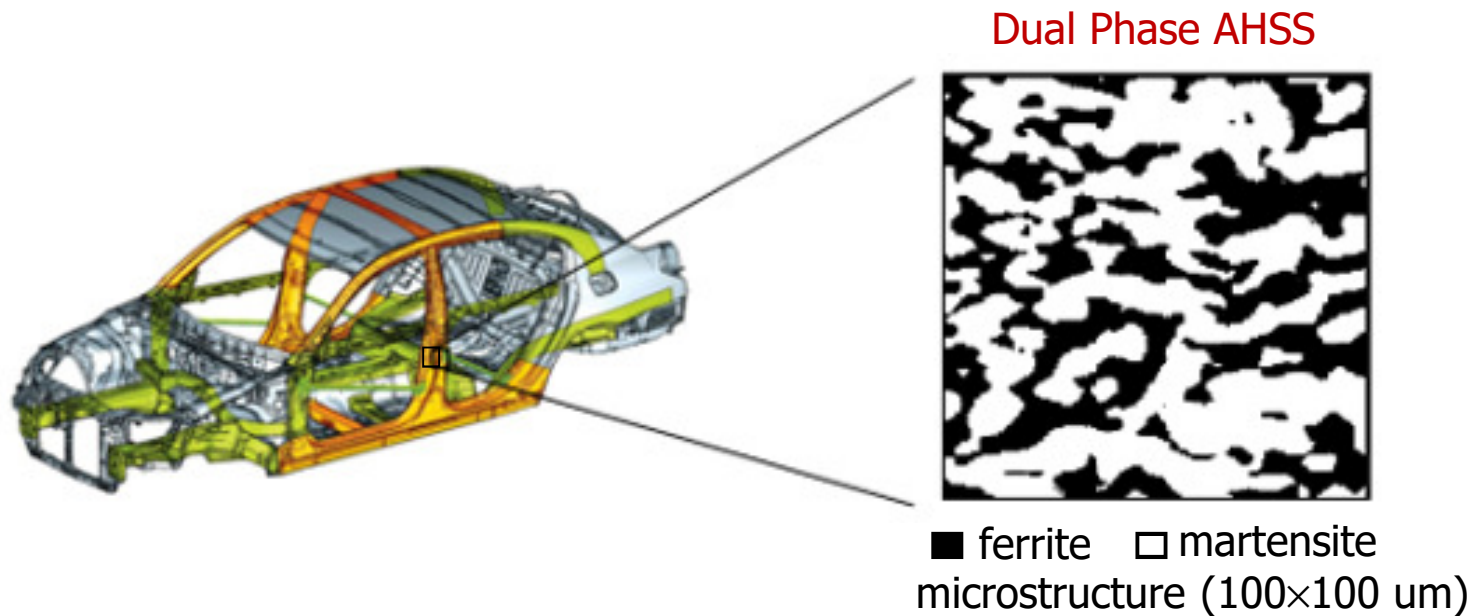
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- Motivation
- State of the art
- Methodology
  - Microstructure information extraction
  - Degradation model incorporating microstructure
  - Reliability analysis and failure prediction
  - Model parameter estimation & statistical inference
- Simulation study
- Case study
- Conclusion

# Introduction

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- Microstructure strongly affect material properties
- Advanced High Strength Steel (AHSS) widely applied with higher strength and reducing weight



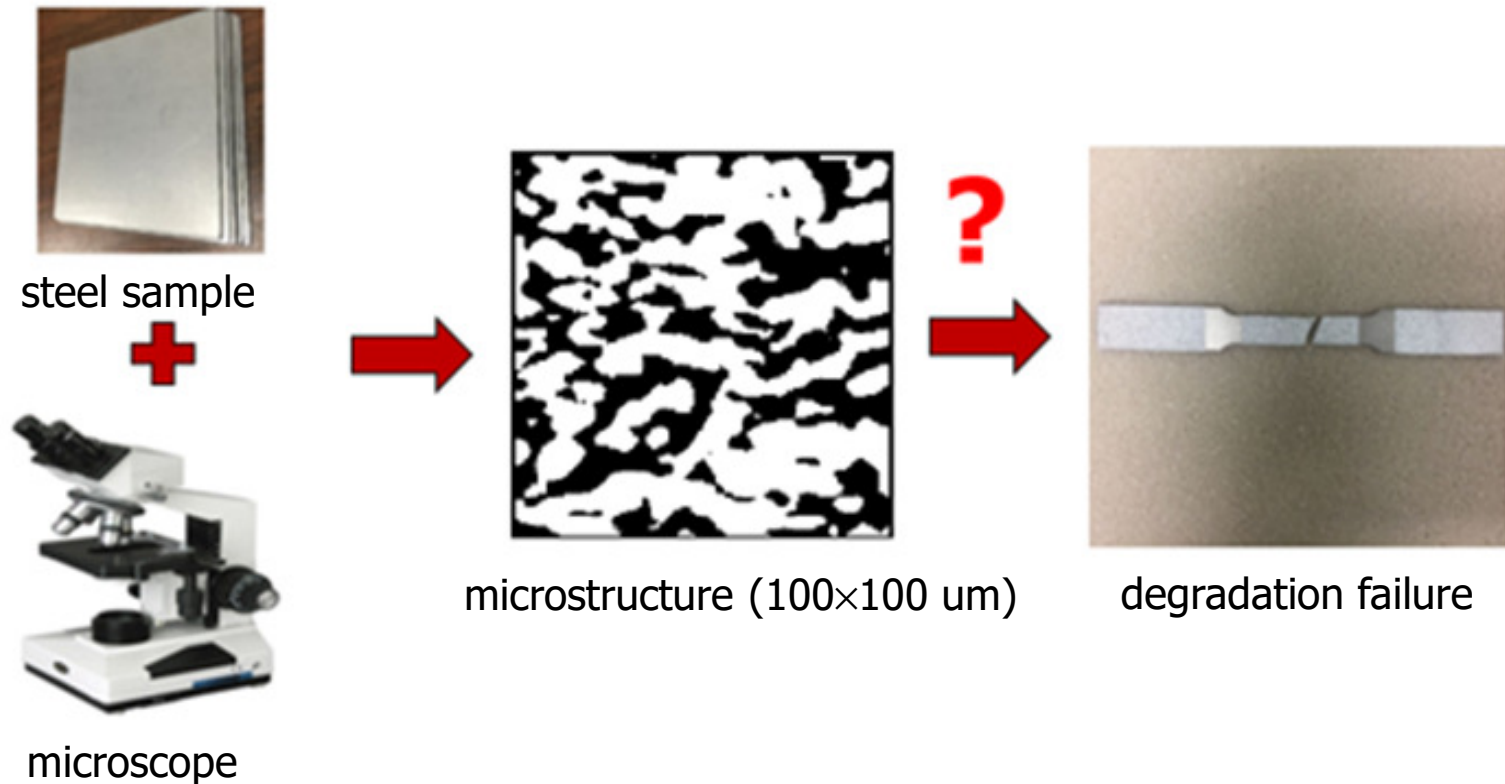
# State of Art

	Materials Science	Failure management
Microstructure	Microstructure images widely obtained from different devices	No use of microstructure
Current research	<ul style="list-style-type: none"><li>• Material property (Callester, 2007, etc)</li><li>• Mechanical property (Torquato, 2013, etc)</li><li>• Material design (Hughus, 2011, etc)</li></ul>	<ul style="list-style-type: none"><li>• Reliability analysis (Meeker et al, 2013, etc)</li><li>• Quality Control (Montgomery, 2010,etc)</li><li>• Optimal maintenance (Kobbacy, et al, 2008, etc)</li></ul>
Limitations	<ul style="list-style-type: none"><li>• Not efficiently describe complex topology and samples variation</li><li>• Not linked to component/system</li></ul>	<ul style="list-style-type: none"><li>• Study in the Macro level</li><li>• Little research consider material microstructure</li></ul>

Little existing research links material microstructure with failure management

# Motivation

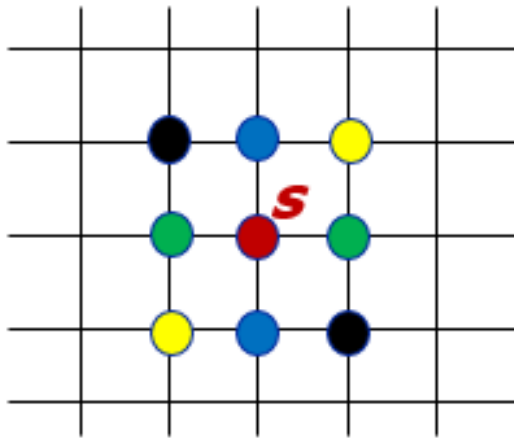
- Material microstructure strongly impacts its degradation



Utilize microstructure image information to capture degradation variability & predict failure more precisely

# Classical Autologistic Regression to Model A Single Microstructure Sample

- Established to model 0-1 type spatial binary data (Gumpertz *et al.*, 1997)
- Defined on a lattice:
  - $s$ : site on the lattice
  - $X_s$ : random variable in  $\{0, 1\}$
  - $N_s$ : a set of neighbor sites

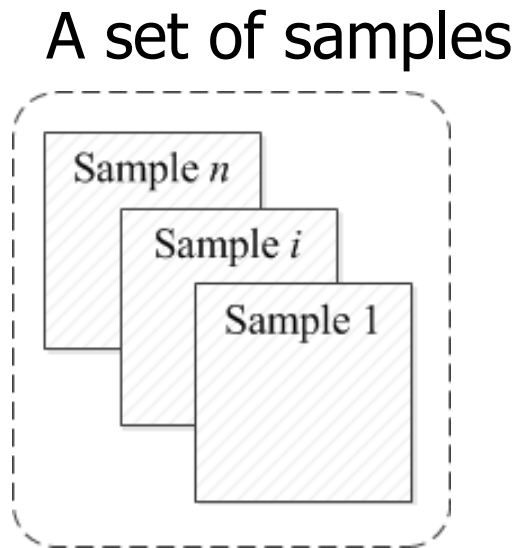


$$\left\{ \begin{array}{l} \Pr(X_s = x_s | X_t = x_t; t \in N(s)) = \frac{\exp(\eta_s \cdot x_s)}{1 + \exp(\eta_s)} \\ \eta_s = \omega_0 + \sum_{t \in N(s)} \omega_t x_t \end{array} \right.$$

each **site** on the lattice corresponds to a **pixel** in the image

# A New Random Effect Autologistic Regression model

- A new model to capture sample variance (Zhang & Yang.,2015)\*



$$\left\{ \begin{array}{l} \Pr(X_{i,s} = x_{i,s} | X_{i,t} = x_{i,t}; t \in N_i(s)) = \frac{\exp(\eta_{i,s} \cdot x_{i,s})}{1 + \exp(\eta_{i,s})} \\ \eta_{i,s} = \omega_{i,0} + \sum_{t=1}^q \omega_{i,t} x_{i,t}; t \in N_i(s) \\ \omega_i = (\omega_{i,0}, \omega_{i,1}, \dots, \omega_{i,q})^T \sim N(\boldsymbol{\mu}, \boldsymbol{\Sigma}) \end{array} \right.$$

*random effect for sample i*

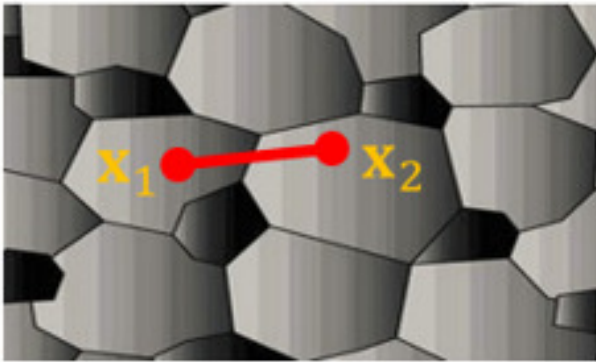
- Stochastic Approximation EM for model parameter estimation

\* Zhang N. and Yang, Q., "A Random Effect Autologistic Regression Model with Application for Characterizing Variation of Multiple Microstructure Samples", *IISE Transactions on Quality and Reliability*, vol, 48 pp 34-42, 2015. (**Industrial Engineering Research Conference Best Student Paper Award**, 2015)

# Statistical Correlation Functions

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- One point correlation function  $S_1^{(j)}(x_1)$ : probability one point in phase  $j$ , i.e., phase volume ratio  $\phi_j$
- Two point correlation function  $S_2^{(j)}(x_1, x_2)$ : probability two points both in phase  $j$ ,



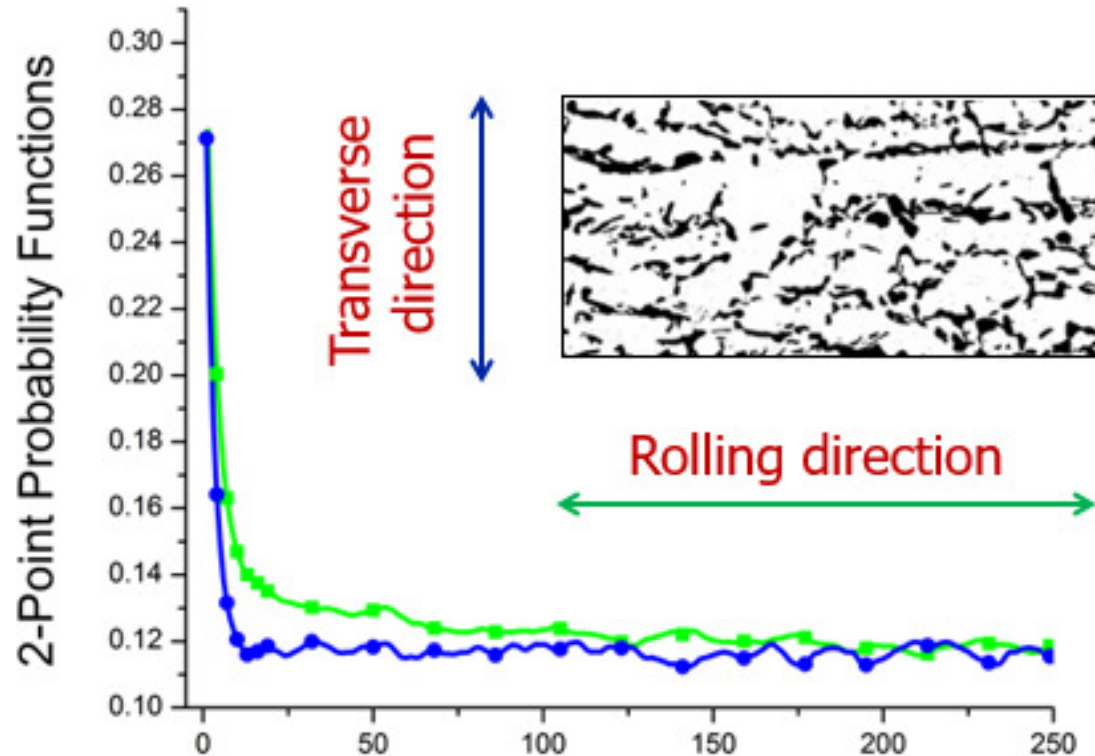
when  $r = |x_1 - x_2|$ , use  $S_2^{(j)}(r)$   
instead of  $S_2^{(j)}(x_1, x_2)$

- $S_2^{(j)}(0) = \phi_j$  and  $\lim_{r \rightarrow \infty} S_2^{(j)}(r) = \phi_j^2; j = 1, 2$



# Deal with Anisotropy

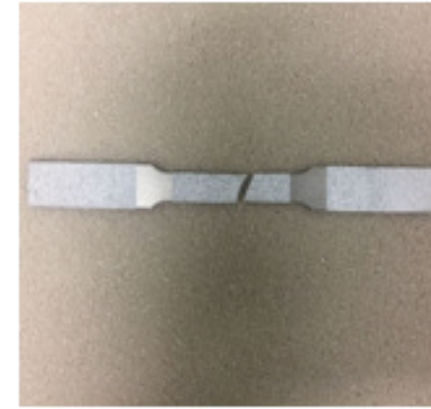
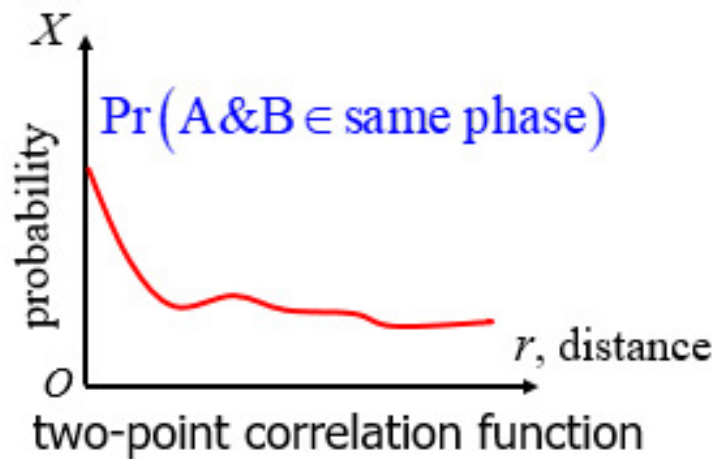
- $S_2^{(j)}(\mathbf{r})$  in two directions:
  - Rolling (horizontal)  $S_{2,h}^{(j)}(\mathbf{r})$  and Transverse (vertical)  $S_{2,v}^{(j)}(\mathbf{r})$



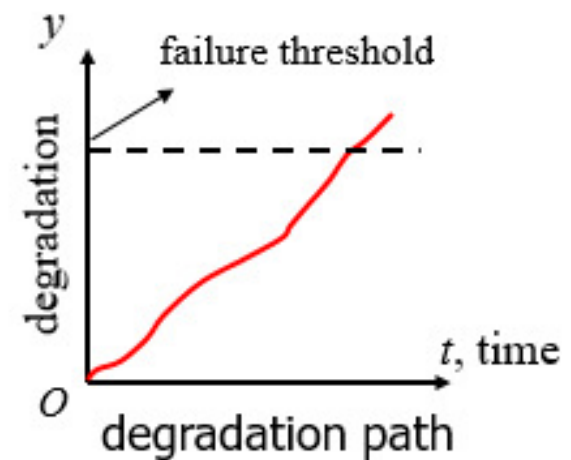
# Framework



microstructure  
information

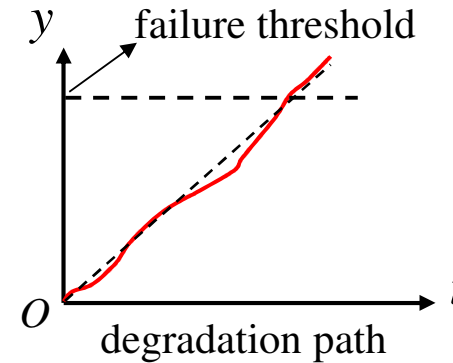
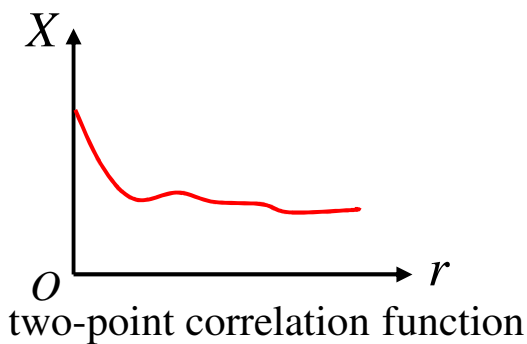


model  
degradation



# A New Functional Covariate Degradation Model

- Microstructure effect on degradation path



- Path function

$$g(y_{ij}) = a_i t_j + b_i + \varepsilon_{ij}; \quad \varepsilon_{ij} \sim N(0, \sigma^2) \Rightarrow \text{linear path}$$

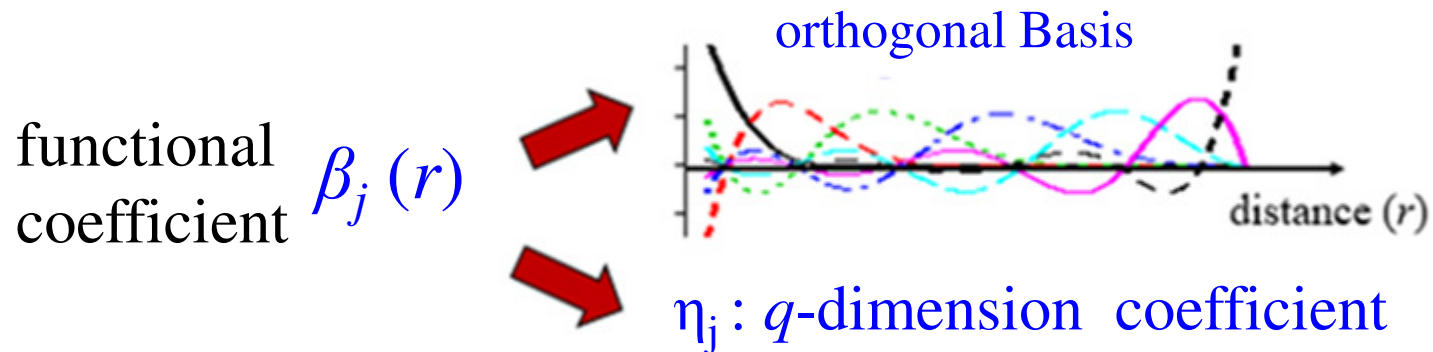
- Microstructure effect

$$\begin{cases} a_i = a_0 + \int_0^\omega \beta_1(r) X_{ic}(r) dr \\ b_i = b_0 + \int_0^\omega \beta_2(r) X_{ic}(r) dr \end{cases} \Rightarrow \text{functional regression}$$

- $X_{ic}(r)$ : centered two-point correlation function
- $\beta_i(r)$ : functional coefficient
- $a_0$  &  $b_0$ : baseline slope & intercept parameters
- $r$ : normalized distance

# Functional Covariate Degradation Model (Cont'd)

- Functional coefficient decomposition



- Degradation function in matrix form

$$\mathbf{y} = \mathbf{Z}\boldsymbol{\theta} + \boldsymbol{\varepsilon}; \quad \boldsymbol{\theta} = (a_0, \boldsymbol{\eta}_1^T, b_0, \boldsymbol{\eta}_2^T)^T$$

- $\mathbf{y} = (\mathbf{y}_1^T, \mathbf{y}_2^T, \dots, \mathbf{y}_n^T)^T$ ; where  $\mathbf{y}_i = (y_{i1}, y_{i2}, \dots, y_{im_i})^T$ : degradation of the  $i^{\text{th}}$  sample
- $\mathbf{Z}$ : design matrix of dimension  $\sum_{i=1}^n m_i \times (2q_n + 2)$ , with  $\left(\sum_{i=1}^n m_{i-1} + j\right)^{\text{th}}$  row being  $t_j \mathbf{x}_{1i}^T + \mathbf{x}_{2i}^T$
- $\mathbf{x}_{1i} = (1, \boldsymbol{\rho}_i^T, 0, \mathbf{0}_{1 \times q_n})^T$ ;  $\mathbf{x}_{2i} = (0, \mathbf{0}_{1 \times q_n}, 1, \boldsymbol{\rho}_i^T)^T$ ;  $\boldsymbol{\rho}_i = (\rho_{i1}, \rho_{i2}, \dots, \rho_{iq_n})^T$ ;  $\rho_{ik} = \int_0^1 X_{ic}(r) b_k(r) dr$
- $m_i$ : # of measurements of the  $i^{\text{th}}$  sample;  $m_0=0$

# Model Dimension Reduction

## ■ Truncation error bound

### ■ Condition 1.

- Functional coefficients are square-integrable:  $\int_0^1 \beta_p^2(r) \leq C_1; p = 1, 2$
- Functional covariate belongs to the Sobolev ellipsoid of order two,

$$\text{i.e., } \sum_{k=1}^{\infty} \rho_{ik}^2 k^4 \leq C_2^2; i = 1, 2, \dots, n; \text{ (Fan, et al. 2015)}$$

- Under Condition 1, the truncation error can be bounded as

$$e_{ij} = \left| E \left( y_{ij} - y_{ij}^* \right) \right| \leq (t_j + 1) C_1^{1/2} C_2 q_n^{-2} = O \left( q_n^{-2} \right)$$

$$\bullet y_{ij}^* = \left( a_0 + \int_0^1 \beta_1(r) X_{ic}(r) dr \right) t_j + b_0 + \int_0^1 \beta_2(r) X_{ic}(r) dr + \varepsilon_{ij} : \text{true degradation}$$

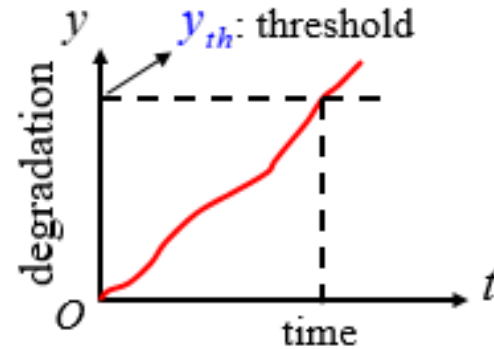
$$\bullet y_{ij} = \left( a_0 + \sum_{k=1}^{q_n} \eta_{1k} \rho_{ik} \right) t_j + b_0 + \sum_{k=1}^{q_n} \eta_{2k} \rho_{ik} + \varepsilon_{ij} : \text{truncated degradation}$$

as  $q_n \rightarrow \infty$ , truncation error  $e_{ij}$  uniformly  $\rightarrow 0$  with order 2

# Reliability Analysis and Prognosis

- Degradation-based reliability

Fail when degradation level reaches threshold value  $y_{th}$



- Distribution of time-to-failure

- ❖ CDF: 
$$F_T(t; \theta) = \Pr(y(t) \geq y_{th}) = 1 - \Phi\left(\frac{y_{th} - \mu(t)}{\sigma}\right)$$

$$= 1 - \Phi\left(\frac{y_{th} - (a_0 + \rho^T \eta_1)t - b_0 - \rho^T \eta_2}{\sigma}\right)$$

- ❖ PDF: 
$$f_T(t; \theta) = dF_T(t; \theta)/dt$$

$$= \frac{(a_0 + \rho^T \eta_1)}{\sigma} \times \phi\left(\frac{y_{th} - (a_0 + \rho^T \eta_1)t - b_0 - \rho^T \eta_2}{\sigma}\right)$$

•  $\Phi(x)$ : CDF of standard normal

•  $\phi(x)$ : PDF of standard normal

# Model Parameter Estimation

- Model parameters:  $\{\boldsymbol{\theta}, \sigma\}$  or  $\{a_0, b_0, \sigma, \beta_1(r), \beta_2(r)\}$
- $\boldsymbol{\theta}$  can have high dimension due to high dimension of functional coefficients
- Penalized least squares estimation (PLSE)
  - minimize the penalized sum of squared errors (PSSE)

$$\hat{\boldsymbol{\theta}} = \arg \min_{\boldsymbol{\theta} \in \mathbb{R}^{2q_n+2}} \{\text{PSSE}(\boldsymbol{\theta})\}$$

where  $\text{PSSE}(\boldsymbol{\theta}) = \boxed{\text{SSE}(\boldsymbol{\theta})} + \boxed{\sum_{p=1}^2 \lambda_p \int_0^\omega \beta_p''(r)^2 dr}$



sum of squared errors



penalty term

# Model Parameter Estimation (Cont'd)

- Estimation of  $\theta$

In the PLSE,  $\theta$  can be derived in a closed-form:

$$\hat{\theta} = (\mathbf{Z}^T \mathbf{Z} + \mathbf{\Omega})^{-1} \mathbf{Z}^T \mathbf{y}$$

- $\mathbf{Z}$ : design matrix
- $\mathbf{y} = (\mathbf{y}_1^T, \mathbf{y}_2^T, \dots, \mathbf{y}_n^T)^T$   
: degradation signals

$$\bullet \mathbf{\Omega} = \begin{bmatrix} \mathbf{0}_{1 \times 1} & \mathbf{0}_{1 \times q_n} & \mathbf{0}_{1 \times 1} & \mathbf{0}_{1 \times q_n} \\ \mathbf{0}_{q_n \times 1} & \lambda_1 \mathbf{\omega} & \mathbf{0}_{q_n \times 1} & \mathbf{0}_{q_n \times q_n} \\ \mathbf{0}_{1 \times 1} & \mathbf{0}_{1 \times q_n} & \mathbf{0}_{1 \times 1} & \mathbf{0}_{1 \times q_n} \\ \mathbf{0}_{q_n \times 1} & \mathbf{0}_{q_n \times q_n} & \mathbf{0}_{q_n \times 1} & \lambda_2 \mathbf{\omega} \end{bmatrix}$$

- $q_n = O(n)$ : # of basis functions
- $\omega_{uv} = \int_0^1 b_u''(r) b_v''(r) dr$

- Choosing smoothing parameters  $\Lambda = \{\lambda_1, \lambda_2\}$

Generalized cross validation (GCV) criterion (Li, 1986) is used

$$\hat{\Lambda} = \arg \min_{\Lambda \in \mathbb{R}^2} \left\{ \frac{(\mathbf{y} - \hat{\mathbf{y}})^T (\mathbf{y} - \hat{\mathbf{y}})}{\left(1 - \frac{\text{trace}(\mathbf{H})}{\sum_{i=1}^n m_i}\right)^2} \right\}$$

- $\mathbf{H} = \mathbf{Z}(\mathbf{Z}^T \mathbf{Z} + \mathbf{\Omega})^{-1} \mathbf{Z}^T$  : hat matrix
- $m_i$ : # of measurements of  $i^{\text{th}}$  sample



# Model Parameter Estimation (Cont'd)

- Estimation of  $\sigma$

Based on  $\hat{\boldsymbol{\theta}}$ ,  $\sigma$  can be calculated as:

$$\hat{\sigma} = \sqrt{\text{SSE}(\hat{\boldsymbol{\theta}})/(N - df)} = \sqrt{(\mathbf{y} - \hat{\mathbf{y}})^T (\mathbf{y} - \hat{\mathbf{y}})/(N - df)}, \quad df = \text{trace}(\mathbf{H})$$

$$\bullet \hat{\mathbf{y}} = \mathbf{Z}(\mathbf{Z}^T \mathbf{Z} + \boldsymbol{\Omega})^{-1} \mathbf{Z}^T \mathbf{y} = \mathbf{H} \mathbf{y} \quad \bullet N: \text{total number of measurements}$$

- Estimation of  $\beta_1(r)$  and  $\beta_2(r)$

Based on  $\hat{\boldsymbol{\theta}}$ ,  $\beta_1(r)$  and  $\beta_2(r)$  can be calculated as:

$$\begin{cases} \hat{\beta}_1(r) = \left(0, \mathbf{B}(r)^T, 0, \mathbf{0}_{1 \times q_n}\right) \hat{\boldsymbol{\theta}} = \left(0, \mathbf{B}(r)^T, 0, \mathbf{0}_{1 \times q_n}\right) (\mathbf{Z}^T \mathbf{Z} + \boldsymbol{\Omega})^{-1} \mathbf{Z}^T \mathbf{y} \\ \hat{\beta}_2(r) = \left(0, \mathbf{0}_{1 \times q_n}, 0, \mathbf{B}(r)^T\right) \hat{\boldsymbol{\theta}} = \left(0, \mathbf{0}_{1 \times q_n}, 0, \mathbf{B}(r)^T\right) (\mathbf{Z}^T \mathbf{Z} + \boldsymbol{\Omega})^{-1} \mathbf{Z}^T \mathbf{y} \end{cases}$$

$$\bullet \mathbf{B}(r) = \left(b_1(r), b_2(r), \dots, b_{q_n}(r)\right)^T \quad \bullet b_i(r) : \text{the } i^{\text{th}} \text{ selected basis function}$$

# Statistical Inference

- Analytical interval estimation of parameters  $\theta$

- Covariance matrix of  $\theta$

$$\text{Var}(\hat{\theta}) = \sigma^2 (\mathbf{Z}^T \mathbf{Z} + \mathbf{\Omega})^{-1} \mathbf{Z}^T \mathbf{Z} (\mathbf{Z}^T \mathbf{Z} + \mathbf{\Omega})^{-T}$$

- 100(1- $\alpha$ )% confidence interval (CI) of  $\theta \in \theta$

$$\left( \hat{\theta} - t_{N-df, \alpha/2} \times \text{SE}(\hat{\theta}), \hat{\theta} + t_{N-df, \alpha/2} \times \text{SE}(\hat{\theta}) \right) \quad \text{SE : standard error}$$

- Analytical interval estimation of parameter  $\sigma$

- An approximation

$$(N - df) \hat{\sigma}^2 / \sigma^2 \sim \chi_{N-df}^2$$

- 100(1- $\alpha$ )% confidence interval of  $\sigma$

$$\text{CI}(\sigma) = \left( \hat{\sigma} \sqrt{(N - df) / \chi_{\alpha/2, N-df}^2}, \hat{\sigma} \sqrt{(N - df) / \chi_{1-\alpha/2, N-df}^2} \right)$$

# Statistical Inference (Cont'd)

- Analytical point-wise interval estimation of  $\beta_1(r)$  and  $\beta_2(r)$ 
  - 100(1- $\alpha$ )% pointwise confidence interval (PCB)

$$\text{PCB}(\beta_p(r)) = \mathbf{B}(r)^T \hat{\boldsymbol{\eta}}_p \mp z_{1-\alpha/2} \sqrt{\mathbf{B}(r)^T \text{Var}(\hat{\boldsymbol{\eta}}_p) \mathbf{B}(r)}; p = 1, 2$$

- Analytical point-wise interval estimation of  $F_T(t; \boldsymbol{\theta})$ 
  - 100(1- $\alpha$ )% pointwise confidence interval

$$\text{PCB}(F_T(t; \boldsymbol{\theta})) = F_T(t; \hat{\boldsymbol{\theta}}) \mp z_{1-\alpha/2} \times \text{SE}(t; \hat{\boldsymbol{\theta}})$$

where  $\text{SE}(t; \hat{\boldsymbol{\theta}}) = \left[ (\nabla F_T(t; \boldsymbol{\theta}))^T \text{Var}(\hat{\boldsymbol{\theta}}) \nabla F_T(t; \boldsymbol{\theta}) \right]^{1/2} \Big|_{\boldsymbol{\theta}=\hat{\boldsymbol{\theta}}}$

$$\begin{aligned} \nabla F_T(t; \boldsymbol{\theta}) &= \nabla \left( 1 - \Phi \left( \frac{y_{th} - (a_0 + \boldsymbol{\rho}^T \boldsymbol{\eta}_1)t - b_0 - \boldsymbol{\rho}^T \boldsymbol{\eta}_2}{\sigma} \right) \right) \\ &= \phi \left( \frac{y_{th} - (a_0 + \boldsymbol{\rho}^T \boldsymbol{\eta}_1)t - b_0 - \boldsymbol{\rho}^T \boldsymbol{\eta}_2}{\sigma} \right) \times \frac{1}{\sigma} [t, t\rho_1, t\rho_2, \dots, t\rho_{q_n}, 1, \rho_1, \rho_2, \dots, \rho_{q_n}]^T \end{aligned}$$

# Simulation Study

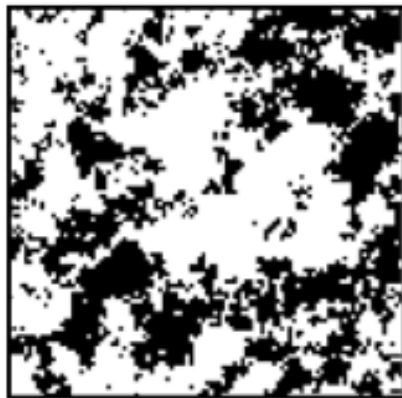
- Data simulation
  - Simulate 100 images and corresponding 100 degradation paths with parameters:

$$a_0 = 1, b_0 = 0.5, \sigma = 0.05$$

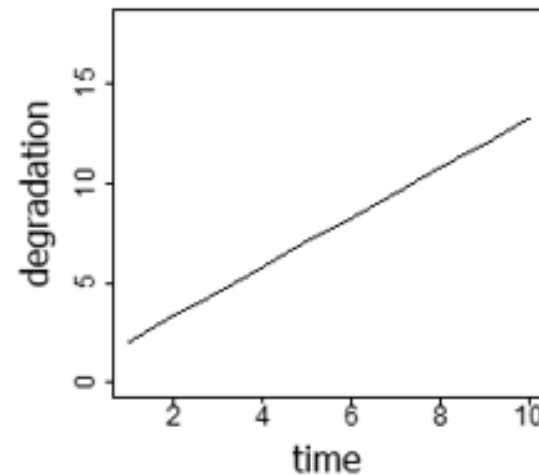
$$\beta_1(r) = 5(\sin(3r) + \cos(5r) + \cos(7r))$$

$$\beta_2(r) = 5(\sin(2r) + \cos(4r) + \cos(6r))$$

A sample image (100x100 pixels)



The corresponding degradation path

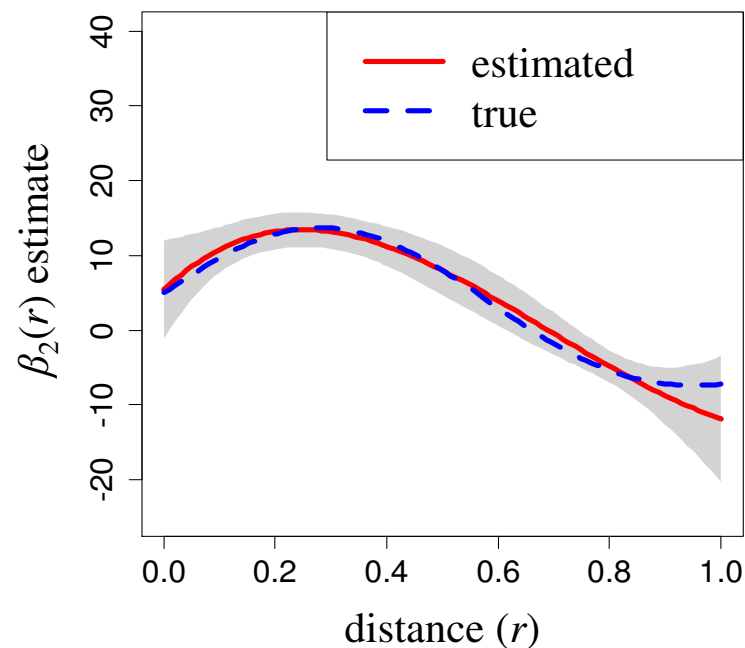
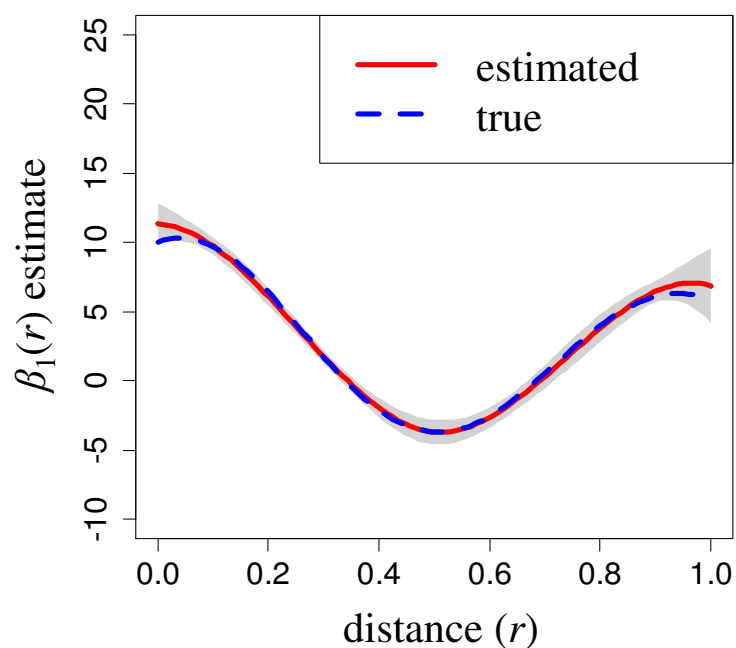


# Simulation Study: Parameter Estimation

- Parameter estimation results ( $q_n=5$ )

Estimates  $\hat{a}_0 = 1.000$ ;  $\hat{b}_0 = 0.499$ ;  $\hat{\sigma} = 0.051$

95% CI (0.999, 1.001); (0.493, 0.505); (0.048, 0.052)



- Estimated parameters are close to true values

# Time-to-failure Prediction

- The proposed model and four benchmark models

Model Index	Model Description
<b>I</b>	<b>The proposed model that uses the two-point correlation function as a predictor</b>
II	Use the phase volume fraction as a scalar predictor
III	Use the exponential covariance function as a functional predictor
IV	Apply functional principal component analysis (FPCA) to the two-point correlation function to extract features as scalar predictors
V	The linear path model (without considering microstructures)

# Time-to-failure Prediction (Cont'd)

- Performance of time-to-failure prediction
  - Root-Mean-Square-Errors (RMSEs) calculated using leave-one-out cross-validation

$$RMSE(T_f | \text{Data}) = \sqrt{\frac{1}{n} \sum_{i=1}^n (\hat{T}_{fi} - T_{fi}^*)^2}$$

Threshold value	RMSEs				
	Model I	Model II	Model III	Model IV	Model V
5	0.03	0.17	0.31	0.06	1.07
15	0.10	0.41	0.86	0.19	2.87
30	0.22	0.79	1.69	0.40	5.56



**Best**



**Third best**



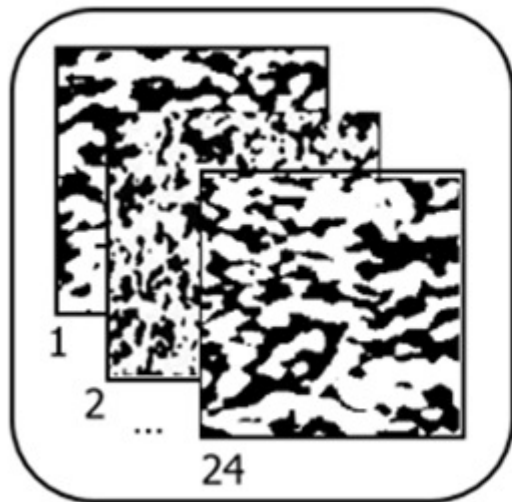
**Second best**



# Case Study

- 24 DP steel samples: 24 microstructure images and the corresponding 24 degradation paths are obtained

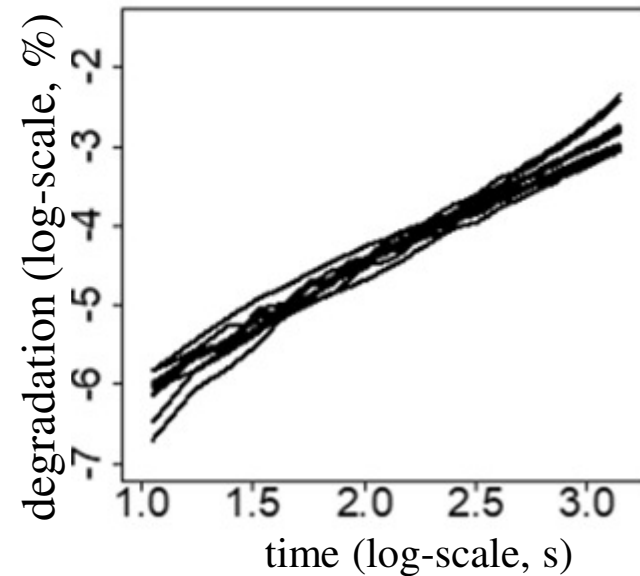
microstructure images



DP steel samples



degradation paths



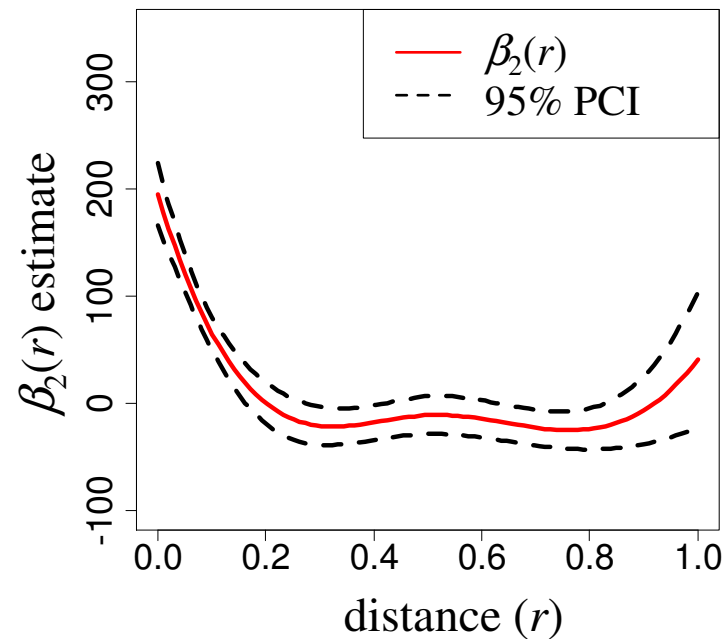
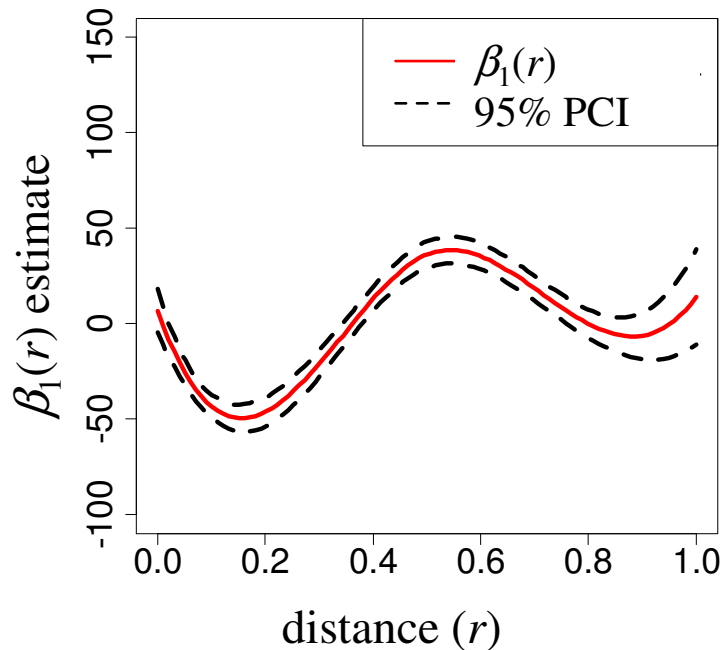
Degradation (deformation) paths are approximately linear after log-log transformation



# Case Study: Parameter Estimation

- Parameter estimation results

Estimates  $\hat{a}_0 = 1.51$ ;  $\hat{b}_0 = -7.81$ ;  $\hat{\sigma} = 0.253$   
95% CI (1.498, 1.522); (-7.844, -7.776); (0.248, 0.259)



- Results are used to life prediction utilizing microstructures

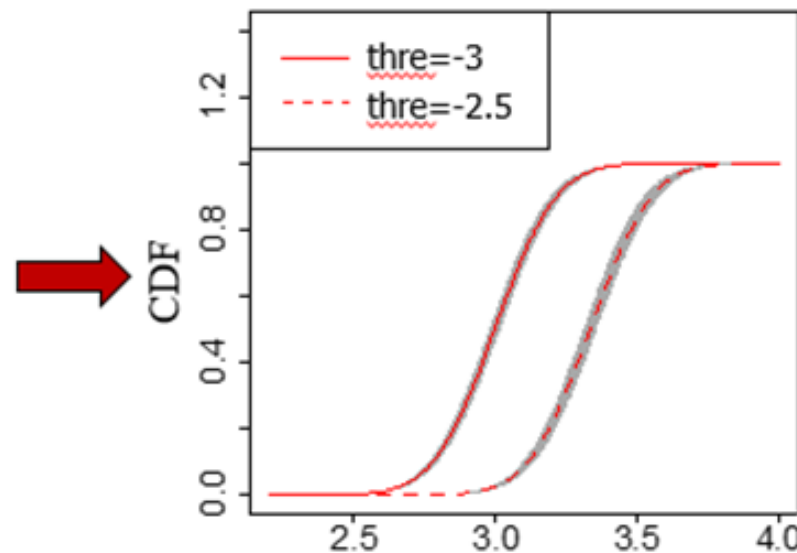
# Case Study: Application Example

- Given a microstructure image, predict the time-to-failure distribution

Microstructure image



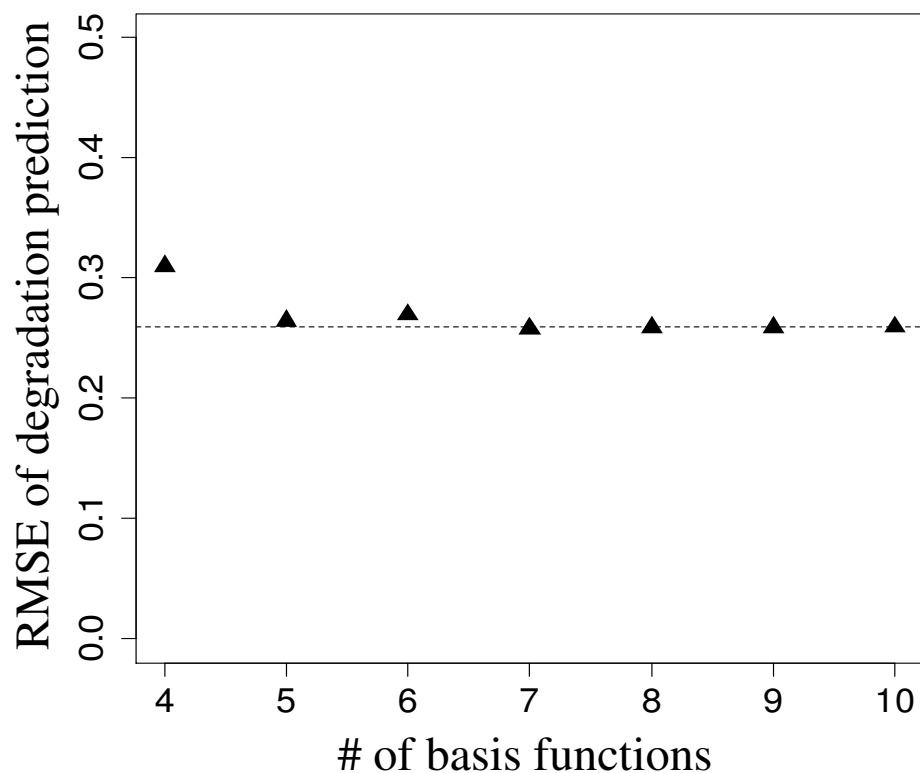
Time-to-failure distribution  
two failure thresholds: -3 and -2.5



- A larger threshold value, a longer expected lifetime

# Case Study: Effect of # of Basis Functions

- Impact of # of basis functions on degradation prediction
  - Calculate the RMSE of degradation path predictions (leave-one-out cross validation)



Choosing five basis functions is sufficient

# Case Study: Model Comparison

- The proposed model and five benchmark models
  - Model VI: power-law path model
  - Calculate the RMSEs (leave-one-out cross validation)

Threshold value	RMSEs					
	Model I	Model II	Model III	Model IV	Model V	Model VI
-4	0.09	0.24	0.31	0.26	0.31	0.30
-3.5	0.12	0.28	0.32	0.29	0.32	0.31

↓                      ↓                      ↓  
**Best**    **Second best**                      **Third best**

The proposed model has the best performance in failure prediction

# Summary

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- Material microstructure can strongly influence material properties
- As the first attempt, a methodology is proposed to efficiently extract material microstructure information, and further incorporate it into material failure management
- A new function degradation model and the corresponding reliability analysis is developed by incorporating material microstructure
- Developed methodology is applied for the advanced high strength duals phase steels
- Physical experiments are designed and conducted to verify the methodology

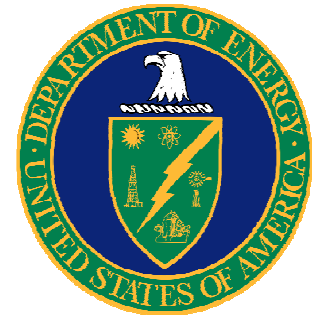
# Acknowledgement

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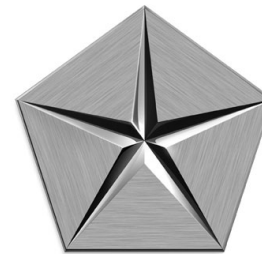
NSF Grant CMMI-1404276 to Wayne State University



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Thank you!

Questions ?

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